


## First Midterm Review


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Mechanical Engineering 483  
**Alternative Energy Engineering II**

March 15, 2010




## Midterm Exam

- Open book and notes
  - No books other than course text
  - No homework solutions or in-class exercise solutions
- Will be problems similar to those on homework and in-class exercise
- More credit for indicating correct approach to solution than for details of algebra or arithmetic




## What is energy

- Dictionary definition
- Capacity to do work
- Energy resources
- Energy and power (energy/time) units
  - Energy units: joules (J), kilowatt-hours (kWh), British thermal units (Btu)
    - 1 Btu = 1055.056 J
  - Power units: watts (W), Btu/hr
    - 1 W = 1 J/s = 3.412 Btu/hr



## Energy Units and Use

- Energy units: 1 Btu = 1055.056 J; 1 W = 1 J/s = 3.412 Btu/hr, 1 quad = 10<sup>15</sup> Btu
- Fuel equivalencies: 1 ft<sup>3</sup> natural gas ≈ 1000 Btu; 1 bbl crude = 5.8 MMBtu; 1 Mtoe oil = 41.868x10<sup>15</sup> J = 0.0387 quads
- World energy production (2006) is 466x10<sup>15</sup> Btu = 466 quads (quadrillion Btu) = 491x10<sup>18</sup> J = 491 exajoules
- World electricity generation (2006) is 18,930 TWh (terawatt hours)




| Energy Information Administration Data on "Heat Rates" |                                       |
|--|---------------------------------------|
| <b>Coal MMBtu/ton</b>                                  | <b>Petroleum Products MMBtu/bbl</b>   |
| Production: 21.070                                     | Motor Gasoline: 5.204                 |
| Consumption: 20.753                                    | Jet Fuel: 5.670                       |
| Coke 27.426  | Distillate Fuel Oil: 5.825            |
| Industrial: 22.489                                     | Residual Fuel Oil: 6.287              |
| Residential and Commercial: 23.880                     | Liquefied Petroleum Gas (LPG): 3.603  |
| Electric Utilities: 20.401                             | Kerosene: 5.670                       |
| <b>Crude Oil MMBtu/bbl</b>                             | <b>Natural Gas Btu/ft<sup>3</sup></b> |
| Production: 5.800                                      | Production, Dry: 1,027                |
| Imports: 5.948   | Consumption: 1,027                    |
| <b>Electricity Consumption:</b> .                      | Non-electric Utilities: 1,028         |
| Btu per kilowatt-hour 3,412                            | Electric Utilities: 1,019             |
|  | Imports: Btu per cubic foot 1,022     |
|  | Exports: Btu per cubic foot 1,006     |

Energy Information Administration (EIA), *Annual Energy Review 2000*, DOE/EIA-0384(2000) (Washington, DC, August 2001)

## Energy Costs

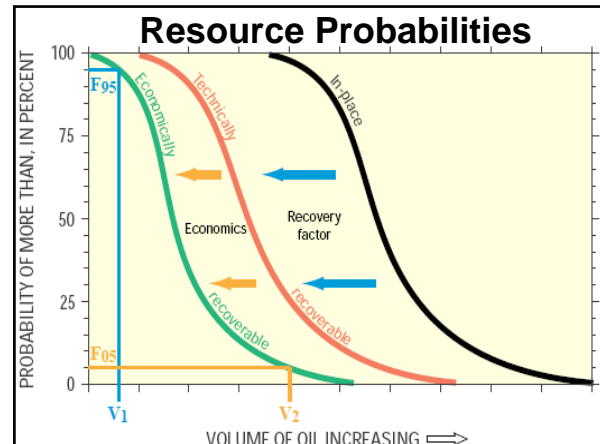
- Home costs (San Fernando Valley 2008)
  - Electricity: \$0.115/kWh = \$32/GJ
    - Increase from \$0.11/kWh to \$0.12/kWh
  - Natural gas: \$1.07/therm = \$11/GJ
    - One therm = 10<sup>5</sup> Btu is approximately the energy in 100 standard cubic feet of natural gas
    - Range was \$0.69 to \$1.22 per therm
  - Gasoline at \$3.00 per gallon (including taxes) costs \$26/GJ
    - Assumes energy content of gasoline is 5.204 MMBtu per (42 gallon) barrel
    - \$100/bbl oil costs \$6.20/GJ (5.80 MMBtu/bbl)
  - Energy cost without California gasoline taxes (\$0.585/gallon) is \$21/GJ



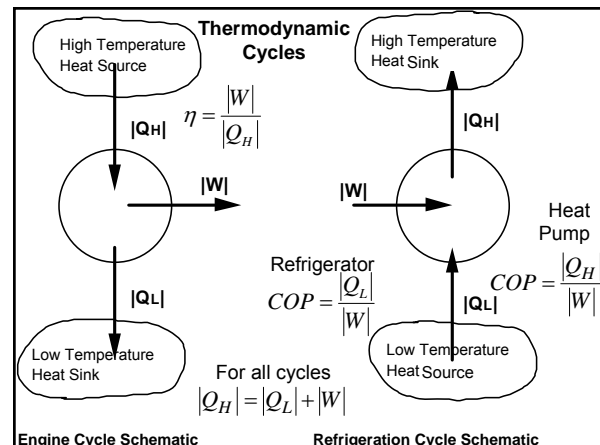
### Resources vs. Reserves

|                           |           |           |
|---------------------------|-----------|-----------|
|                           | Known     | Unknown   |
| Economical to Recover     | Reserves  | Resources |
| Not economical to recover | Resources | Resources |

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- ### Hubbert Peak
- Analysis due to M. King Hubbert
  - Main publications in 1949 and 1956
  - Correctly predicted peak in US oil production in early 1970s
  - Not so accurate in other predictions
  - Some recent applications show world oil production peak in next ten years
  - Many other studies show later peak
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- ### Some Cycles
- Rankine cycle – steam power plant
  - Brayton cycle – gas turbine engines
  - Combined cycle – combination of Brayton and Rankine cycle
  - Otto and Diesel cycles for reciprocating engines
  - Air standard cycles *versus* consideration of heat addition from fuel
  - Refrigerator *versus* heat pump
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- ### Basic Combustion Analysis
- General fuel formula:  $C_xH_yS_zO_wN_v$
  - $x, y, z, w,$  and  $v$  from ultimate analysis or analysis of gas mixtures
  - Ultimate analyses:
    - $x = \text{wt}\%C/12.0107, y = \text{wt}\%H/1.00794,$
    - $z = \text{t}\%S/32.065, w = \text{wt}\%O/16.0004,$
    - $v = \text{wt}\%N/14.0067, m_{\text{fuel}} = 100$
    - $M_{\text{fuel}} = 12.0107x + 1.00794y + 32.065z + 15.9994w + 14.0067v = m_{\text{fuel}}(1 - \%MM)$
  - For mixture of compounds ( $\omega_k = \text{mole fraction}$ )
 
$$x = \sum_{\text{species}} \omega_k x_k \quad y = \sum_{\text{species}} \omega_k y_k \quad M_{\text{fuel}} = \sum_{\text{species}} \omega_k M_k$$
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### Combustion Air

- $A = x + y/4 + z - w/2 =$  stoichiometric moles  $O_2$ /mole fuel
- Need input data on Actual  $O_2$ /Stoichiometric  $O_2 =$  Relative air/fuel ratio  $= \lambda$
- Air/fuel ratio  $= m_{air}/m_{fuel} = 138.28\lambda A/m_{fuel}$
- $C_xH_yS_zO_wN_v + \lambda A(O_2 + 3.77 N_2) \rightarrow xCO_2 + (y/2)H_2O + zSO_2 + (\lambda - 1)AO_2 + 3.77\lambda A + v/2)N_2$

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### Exhaust Oxygen and $\lambda$

- Can relate these two quantities with fuel properties
- Can compute theoretical  $\%O_2$  for given  $\lambda$
- Dry exhaust has water removed to protect chemical analyzers

$$\frac{\%O_2|_{dry}}{100} = \frac{(\lambda - 1)A}{x + 4.77\lambda A - A + z + \frac{v}{2}}$$

$$\lambda = \frac{A + \frac{\%O_2|_{dry}}{100} \left[ x - A + z + \frac{v}{2} \right]}{A \left( 1 - 4.77 \frac{\%O_2|_{dry}}{100} \right)}$$

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### Emission Rates

- Often stated as pollutant mass per unit heat input from fuel
- Equation used:  $E_i = \rho_{i,d} F_d \frac{20.9}{20.9 - \%O_{2,d}}$
- Compute  $\rho_{i,d} = y_{i,d} M_i P_{std} / R_u T_{std}$
- $F_d$  is dry exhaust volume/heat input
  - Use default values or compute by equation
  - Feb 3 notes have values of K's and default  $F_d$ 's

$$F_d = \frac{K(K_C \%C + K_H \%H + K_O \%O + K_S \%S + K_N \%N)}{Q_c}$$

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### Other Equations

- Pollutant mass per unit heat input

$$\frac{m_{CO_2}}{Q_{fuel}} = \frac{3.6642 \text{ wt\% } C}{Q_c} \frac{1}{100} \quad \frac{m_{SO_2}}{Q_{fuel}} = \frac{1.9979 \text{ wt\% } S}{Q_c} \frac{1}{100}$$

- Combustion Efficiency (definitions on next slide)

$$\eta_{comb} = \frac{|q|}{|q|_{max}} = 1 - \frac{\left[ 1 + \frac{Air}{Fuel} \right] \int_{T_m}^{T_{out}} c_{p,Air} dT' - \frac{x f \Delta h_{CO}}{M_{fuel} Q_c}}$$

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### Combustion Efficiency

- Air/fuel is the air to fuel (mass) ratio
- $C_{p,air} = 0.24 \text{ Btu/lb}_m \cdot R = 1.005 \text{ kJ/kg} \cdot K$
- $f =$  molar exhaust ratio  $CO/(CO + CO_2)$
- $x =$  carbon atoms in fuel formula,  $C_xH_y \dots$
- $Q_c =$  heat of combustion (Btu/lb<sub>m</sub> or kJ/kg)
  - Use lower heating value for water vapor (usual case)
- $\Delta h_{CO} = 282,990 \text{ kJ/kgmol} = 121,665 \text{ Btu/lbmol}$
- $M_{fuel}$  is combustible fuel molar mass lb<sub>m</sub>/lbmol or kg/kmol

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### Energy Economics

- Look at balance between initial cost and ongoing costs
  - Uses interest rate to consider time value of money
- Key formula relates equivalence between initial cost, P (present value), and ongoing payment stream, A (annual cost)

$$\frac{A}{P} = \frac{i}{1 - (1+i)^{-n}} \quad \frac{P}{A} = \frac{1 - (1+i)^{-n}}{i}$$

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### Using the A/P formula

- Formula applies to any time period so long as  $i$  is interest rate per time period
- *E. g.*, for monthly costs with  $i = 6\%/yr = 0.5\%/month$  for  $N$  months 
$$A/P = \frac{0.5}{1 - (1 + 0.5)^{-N}}$$
- Need trial-and-error solution (or financial calculator) to find  $i$ , given  $n$  and  $A/P$
- Can find  $n$  for given  $i$  and  $A/P$  
$$n = -\frac{\ln\left(1 - \frac{Pi}{A}\right)}{\ln(1+i)}$$

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### Two Approaches

- Determine present worth of ongoing costs and add to initial costs
  - Total present worth = Initial Cost + (Ongoing Annual Costs)( $P/A$ )
- Determine annualized equivalent of initial cost and add to ongoing costs
  - Total annual costs = Ongoing Annual Costs + (Initial Cost)( $A/P$ )
- Power plant homework example
  - Initial  $C$  \$/kW, Fuel  $F$  \$/MMBtu, O&M  $M$  \$/kWh/yr,  $CF$  = capacity factor,  $HR$  = heat rate MMBtu/kWh,  $E$  = income \$/kWh

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### Electricity Cost Present Worth

- Assume size  $S$  in kW; annual power production,  $PP = 8766 S(CF)$  kWh
  - Initial capital cost =  $CS$
  - O&M present worth =  $M(PP)(P/A)$
  - Fuel present worth  $F(PP)(HR)(P/A)$
  - Electricity sales present worth =  $E(PP)(P/A)$
  - For desired return  $i$  in  $P/A$  formula
    - $CS + M(PP)(P/A) + F(PP)(P/A)(HR) = E(PP)(P/A)$

$$E = \frac{CS}{8766(CF)(P/A)} + M + F(HR) = \frac{C(A/P)}{8766(CF)} + M + F(HR)$$

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### Annualized Electricity Cost

- Assume size  $S$  in kW; annual power production,  $PP = 8766 S(CF)$  kWh
  - Annualized capital cost =  $CS(A/P)$
  - Annual O&M cost =  $M(PP)$
  - Annual fuel cost =  $F(PP)(HR)$
  - Annual electricity sales =  $E(PP)$
  - For desired return  $i$  in  $P/A$  formula
    - $CS(A/P) + M(PP) + F(PP)(HR) = E(PP)$

$$E = \frac{CS(A/P)}{8766(CF)} + M + F(HR) = \frac{C(A/P)}{8766(CF)} + M + F(HR)$$

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### Subtle Point

- In the  $A/P$  formula for  $N$  years
  - The payment  $A$  is done at year end
- For homework problem comparing incandescent and compact fluorescent
  - Compact fluorescent lifetime is 9 years
  - Incandescent lifetime is 1 year
  - Present worth comparison over 9 years
    - $IC$  = initial cost;  $AEC$  = annual electricity cost

$$P_i = IC_i \left(1 + \frac{1 - (1+i)^{-9}}{i}\right) + AEC_i \frac{1 - (1+i)^{-9}}{i} \quad P_{CF} = IC_{CF} + AEC_{CF} \frac{1 - (1+i)^{-9}}{i}$$

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### Payback Period

- Defined as initial cost in dollars divided by annual savings (or income) in dollars per year
- Simplified analysis of fixed cost versus annual savings
- Engineering economics texts recommend **not** using this measure
- But – it is easier to understand than the discount rate

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### Environmental Aspects

- Multimedia impacts from energy use, development, production, refining
- Air pollution
  - Troposphere: O<sub>3</sub>, CO, NO<sub>x</sub>, SO<sub>x</sub>, toxics
  - Stratosphere: CFC's reduce ozone layer
  - Global warming: CO<sub>2</sub>, N<sub>2</sub>O, CH<sub>4</sub>, etc.
- Carbon capture and sequestration
  - Remove CO<sub>2</sub> from energy use and bury it underground

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### Energy Storage Measures

- Energy per unit mass (kJ/kg; Btu/lb<sub>m</sub>)
- Energy per unit volume (kJ/m<sup>3</sup>; Btu/ft<sup>3</sup>)
- Rate of delivery of energy to and from storage (kW/kg; Btu/hr-lb<sub>m</sub>)
- Efficiency (energy out/energy in)
- Life cycles – how many times can the storage device be used
  - Particularly important for batteries

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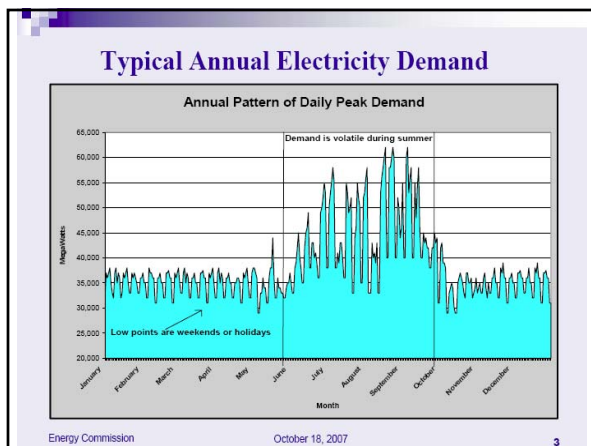
### Fuel Energy

- Volumetric energy storage in Btu/gallon
  - Gasoline: 109,000 to 125,000
  - Diesel fuel: 128,000 to 130,000
  - Biodiesel: 117,000 to 120,000
  - Natural gas: 33,000 to 38,000 at 3,000 psi, 38,000 to 44,000 at 3,600 psi, and ~73,500 as liquefied natural gas (LNG)
  - 85% ethanol in gasoline: ~80,000
  - 85% methanol in gasoline: 56,000 to 66,000
  - Hydrogen: ~6,500 at 3,000 psi, ~16,000 at 10,000 psi, and ~30,500 as liquid
  - Liquefied petroleum gas (LPG): ~84,000

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[http://www.eere.energy.gov/afdc/altfuel/fuel\\_comp.html](http://www.eere.energy.gov/afdc/altfuel/fuel_comp.html)

**Compare**  
 Batteries versus other motive power  
<http://www.nap.edu/books/0309092612/html/40.html>

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| Storage Technologies           | Main Advantages (Relative)                          | Disadvantages (Relative)                                | Power Application | Energy Application |
|--------------------------------|---|---|-------------------|--------------------|
| Pumped Storage                 | High Capacity, Low Cost                             | Special Site Requirement                                |                   | ●                  |
| CASB                           | High Capacity, Low Cost                             | Special Site Requirement, Need Gas Fuel                 |                   | ●                  |
| Flow Batteries: PFB, VFB, ZnBr | High Capacity, Independent Power and Energy Ratings | Low Energy Density                                      | ○                 | ●                  |
| Metal-Air                      | Very High Energy Density                            | Electric Charging is Difficult                          |                   | ●                  |
| NaS                            | High Power & Energy Densities, High Efficiency      | Production Cost, Safety Concerns (addressed in design)  | ●                 | ●                  |
| Li-ion                         | High Power & Energy Densities, High Efficiency      | High Production Cost, Requires Special Charging Circuit | ●                 | ○                  |
| Ni-Cd                          | High Power & Energy Densities, High Efficiency      |   | ●                 | ○                  |
| Other Advanced Batteries       | High Power & Energy Densities, High Efficiency      | High Production Cost                                    | ●                 | ○                  |
| Lead-Acid                      | Low Capital Cost                                    | Limited Cycle Life when Deeply Discharged               | ●                 | ○                  |
| Flywheels                      | High Power  | Low Energy density                                      | ●                 | ○                  |
| SMES, DSMES                    | High Power  | Low Energy Density, High Production Cost                | ●                 |                    |
| S.C. Capacitors                | Long Cycle Life, High Efficiency                    | Low Energy Density                                      | ●                 | ○                  |

**Store**

- Symbols
  - fully capable
  - reasonable
  - feasible, but not quite...
  - not feasible

• [http://www.electrictystorage.org/tech/technologies\\_comparisons.htm](http://www.electrictystorage.org/tech/technologies_comparisons.htm)

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### Renewable/Alternative

- Alternative or renewable resources
  - Solar energy
  - Wind energy
  - Ocean energy (tides, waves and temperature gradients)
  - Geothermal energy
  - Hydropower especially small hydro
  - Biomass fuels
  - Conservation as an alternative resource
    - Reduced usage and improved efficiencies including vehicle fuel economy

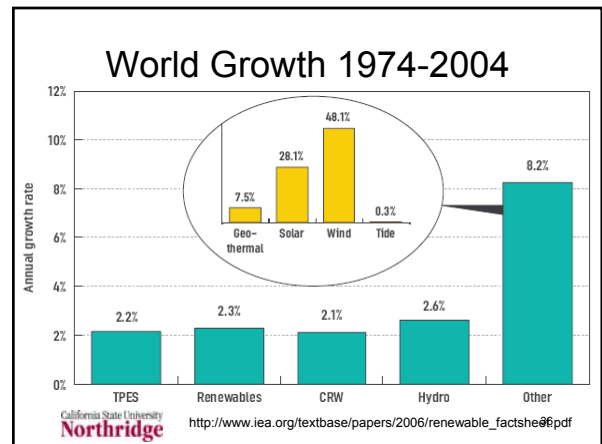
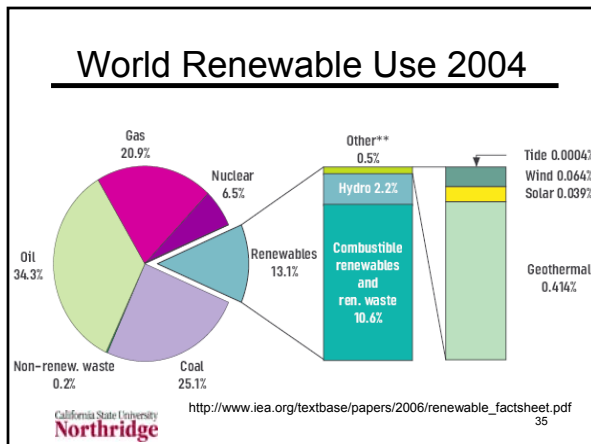
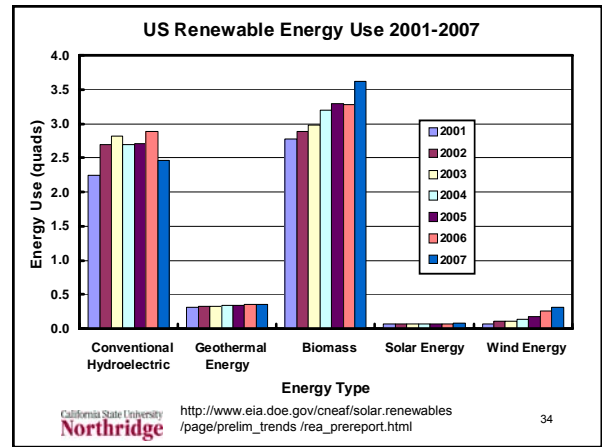
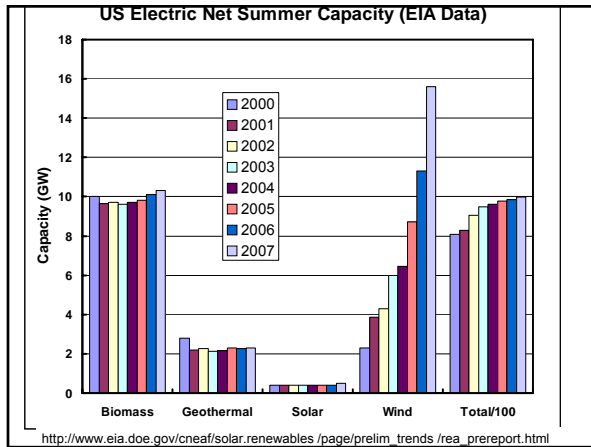
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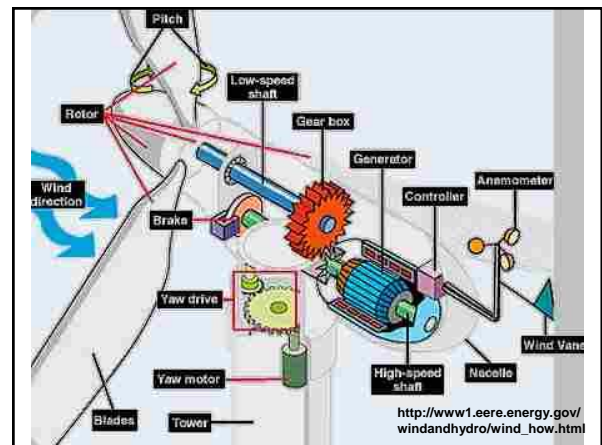
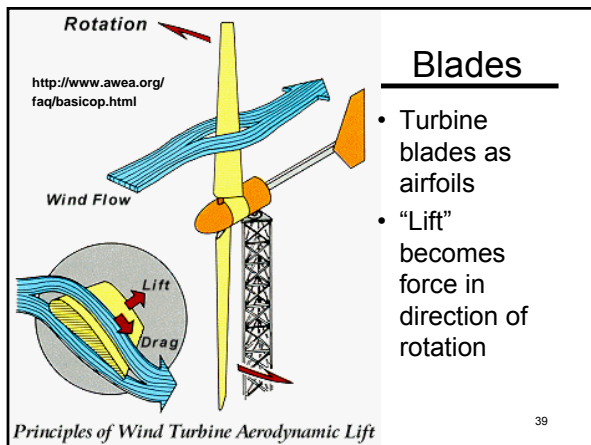
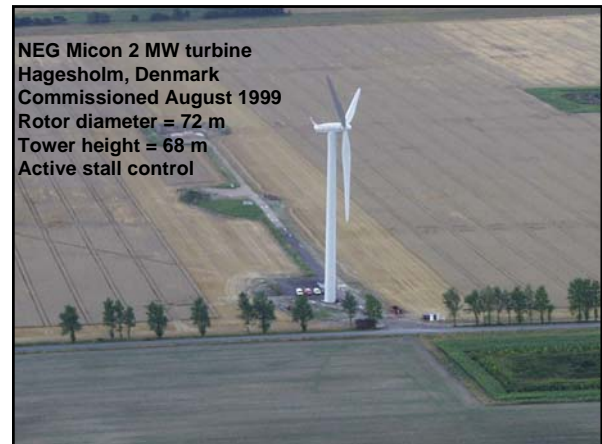
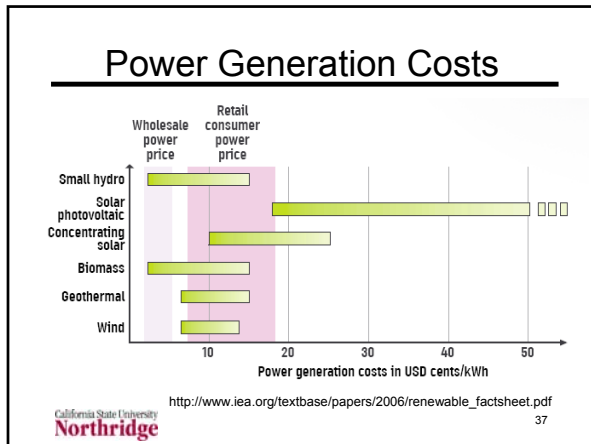
### US Renewable Use 2006

Total = 99.960 Quadrillion Btu      Total = 6.844 Quadrillion Btu

- Solar + geothermal + wind = 10% of renewables = 0.7% of total energy

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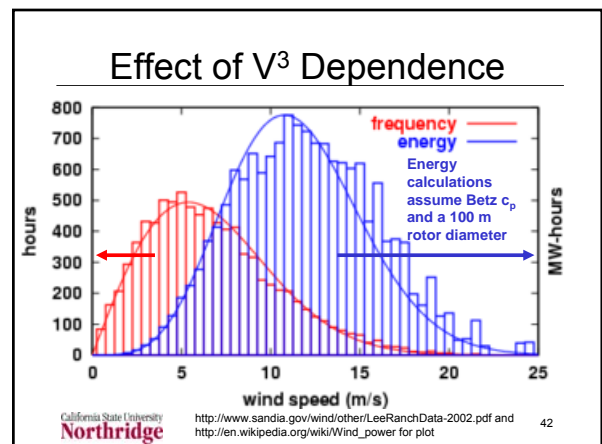


### Wind Power and Betz Limit

- Power in incoming air =  $\dot{m}e = \dot{m}V^2/2 = (\rho VA)V^2/2 = \rho AV^3/2 = P_0$ 
  - Air density,  $\rho \approx 1.2 \text{ kg/m}^3$
  - A = swept area of rotor =  $\pi(D_{\text{rotor}})^2/4$
  - V = wind velocity
- $c_p$  = power coefficient = turbine power divided by power in wind
  - Alternative: (generator power) / (wind power)
- Betz Limit: Maximum theoretical  $c_p = 16/27 \approx 0.593$

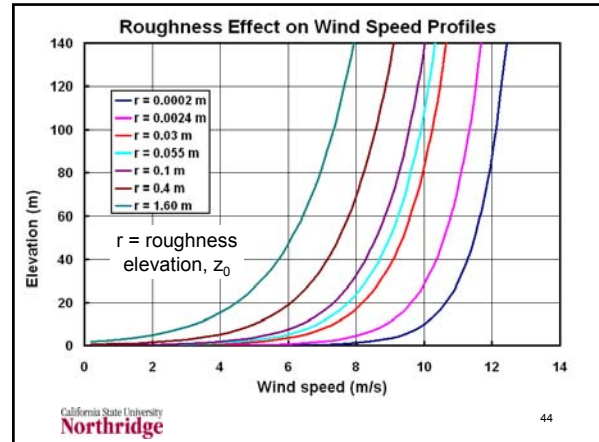
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41



### Roughness Parameters

- Open water ( $r = 0.0002 \text{ m}$ )
- Completely open terrain with smooth surface ( $r = 0.0024 \text{ m}$ )
- Agricultural area varying amounts of fences, hedgerows, buildings ( $r = 0.03 \text{ m}$ ,  $0.055 \text{ m}$ ,  $0.1 \text{ m}$ ,  $0.2 \text{ m}$ )
- Small villages ( $r = 0.4 \text{ m}$ )
- Larger cities with tall buildings ( $r = 0.8 \text{ m}$ )
- Very large cities/skyscrapers ( $r = 1.6 \text{ m}$ )



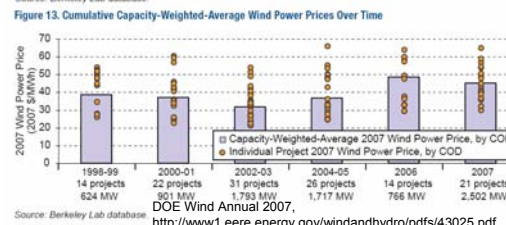
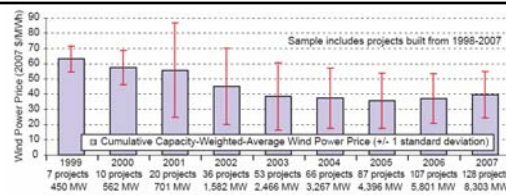
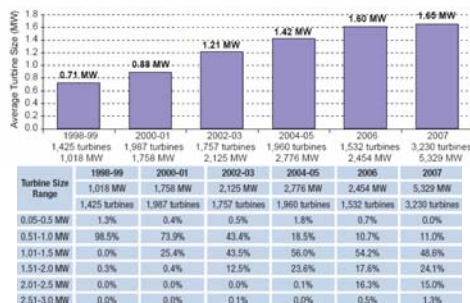
### Wind Classes (10 m)

| Class | power/area(W/m <sup>2</sup> ) |      | Speed(m/s)/(mph) |          |
|-------|-------------------------------|------|------------------|----------|
|       | min                           | max  | min              | max      |
| 1     | 0                             | 100  | 0                | 4.4/9.8  |
| 2     | 100                           | 150  | 4.4/9.8          | 5.1/11.5 |
| 3     | 150                           | 200  | 5.1/11.5         | 5.6/12.5 |
| 4     | 200                           | 250  | 5.6/12.5         | 6.0/13.4 |
| 5     | 250                           | 300  | 6.0/13.4         | 6.4/14.3 |
| 6     | 300                           | 400  | 6.4/14.3         | 7.0/15.7 |
| 7     | 400                           | 1000 | 7.0/15.7         | 9.4/21.1 |

### Wind Classes (50 m)

| Class | power/area(W/m <sup>2</sup> ) |      | Speed(m/s)/(mph) |           |
|-------|-------------------------------|------|------------------|-----------|
|       | min                           | max  | min              | max       |
| 1     | 0                             | 200  | 0                | 5.6/12.5  |
| 2     | 200                           | 300  | 5.6/12.5         | 6.4/14.3  |
| 3     | 300                           | 400  | 6.4/14.3         | 7.0/15.7  |
| 4     | 400                           | 500  | 7.0/15.7         | 7.5/16.8  |
| 5     | 500                           | 600  | 7.5/16.8         | 8.0/17.9  |
| 6     | 600                           | 800  | 8.0/17.9         | 8.8/19.7  |
| 7     | 800                           | 2000 | 8.8/19.7         | 11.9/26.6 |

### Turbine Size History





### Probability Distributions

- Probability distribution function,  $f$ 
  - Probability that the random variable  $x$  lies in a certain range  $a \leq x \leq b$  is integral of pdf

$$P(a \leq x \leq b) = \int_a^b f(x) dx \quad \int_{x_{\min}}^{x_{\max}} f(x) dx = 1$$

- Cumulative distribution function,  $F$ 

$$F(b) = P(x \leq b) = \int_{x_{\min}}^b f(x) dx$$

$$P(a \leq x \leq b) = F(b) - F(a)$$

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### Rayleigh Distribution

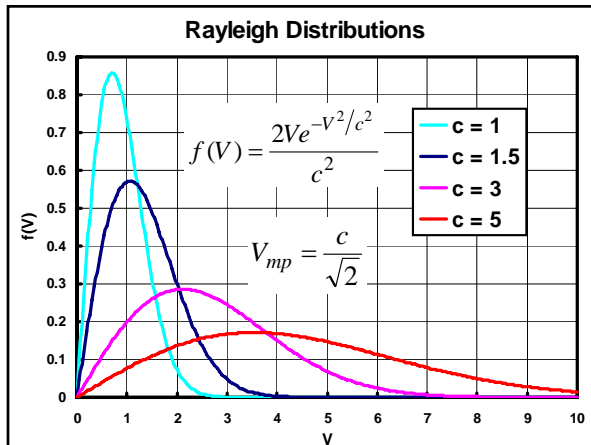
- At least three variations are used

$$V_{mp} = \beta = \frac{c}{\sqrt{2}} \quad f(V) = \frac{V e^{-V^2/2\beta^2}}{\beta^2} \quad 0 \leq V < \infty$$

$$2\beta^2 = c^2 \quad f(V) = \frac{2V e^{-V^2/c^2}}{c^2} \quad 0 \leq V < \infty$$

$$\bar{V} = \beta \sqrt{\frac{\pi}{2}} = \frac{c}{2} \sqrt{\pi} \quad f(V) = \frac{\pi V e^{-\pi V^2/4\bar{V}^2}}{2\bar{V}} \quad 0 \leq V < \infty$$

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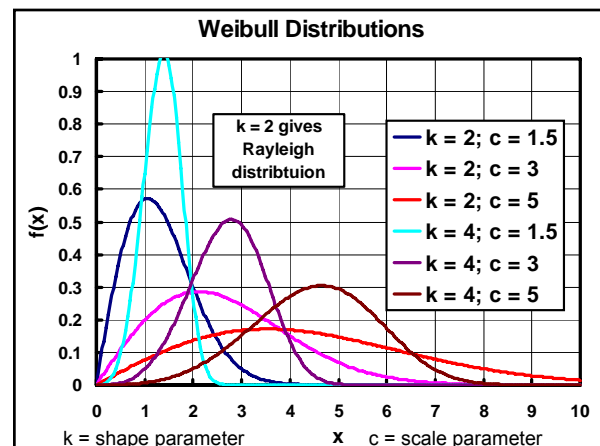
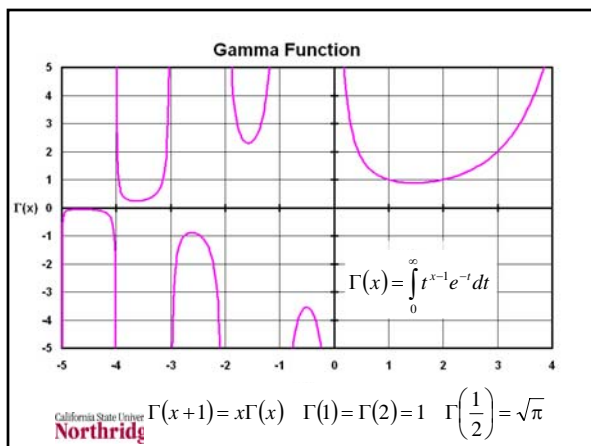
### Weibull Distribution

- A two-parameter distribution with shape parameter,  $k$ , and scale parameter,  $c$
- Rayleigh distribution is Weibull distribution with  $k = 2$
- Mean =  $c\Gamma(1 + k^{-1})$
- Variance =  $c^2[\Gamma(1 + 2k^{-1}) - \Gamma^2(1 + k^{-1})]$

$\Gamma$  is the gamma function

$$f(V) = \frac{k}{c} \left(\frac{V}{c}\right)^{k-1} e^{-(V/c)^k} \quad 0 \leq V < \infty$$

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### Wind Power

- Instantaneous wind power:  $P_0 = \rho V^3 A / 2$
- Total or average wind power:  $\bar{P}_0 = \frac{\rho A V^3}{2} = \frac{\rho A}{2} \int_0^\infty V^3 f(V) dV$
- Total or average turbine power:  $\bar{P}_{total} = c_p \bar{P}_0 = c_p \rho A \bar{V}^3 / 2$

$$\left(\bar{V}^3\right)_{Weibull} = c^3 \Gamma\left(\frac{3}{k} + 1\right)$$

$$\left(\bar{V}^3\right)_{Rayleigh} = c^3 \Gamma\left(\frac{3}{2} + 1\right) = c^3 \frac{3}{2} \Gamma\left(\frac{3}{2}\right) = c^3 \frac{3}{2} \frac{1}{2} \Gamma\left(\frac{1}{2}\right) = c^3 \frac{3\sqrt{\pi}}{4}$$

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### Wind Power Distribution

- Wind power between  $V_1$  and  $V_2$ 
  - Weibull (Set  $k = 2$  for Rayleigh)

$$\text{Wind } \bar{P} \text{ between } V_1 \text{ and } V_2 = \frac{\rho A c^3}{2} \int_{(V_1/c)^k}^{(V_2/c)^k} y^{\frac{3}{k}-1} e^{-y} dy$$

- Found by numerical integration with results in tables

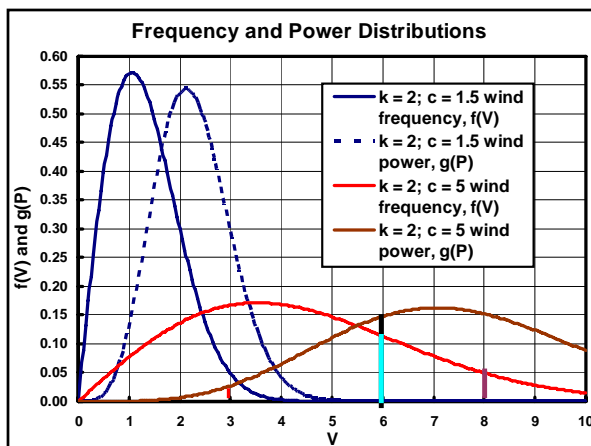
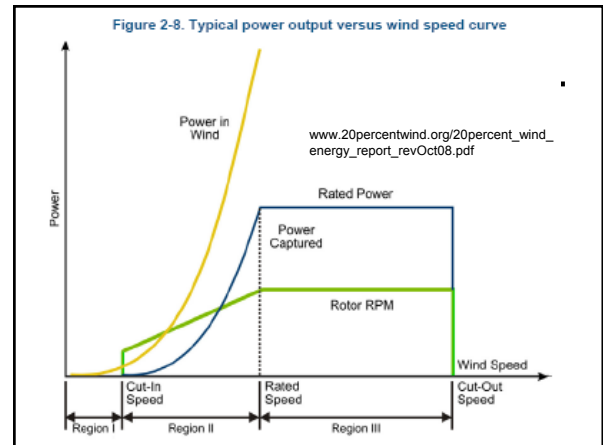
$$\left[ \text{Wind } \bar{P} \text{ between } V_1 \text{ and } V_2 \right] = [f_P(V_2) - f_P(V_1)] \frac{\rho A c^3}{2} \Gamma\left(\frac{3}{k} + 1\right)$$

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### Wind Turbine Operation

- No operation until wind velocity reaches a minimum called the cut-in velocity
- Then operate at full turbine output power until turbine output is greater than generator can accept
- Limit turbine output power to full generator power at high wind speeds
- No operation above maximum velocity called cut-out velocity

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### Average Operating Power

- Generator uses turbine power between  $V_{cut-in}$  and rated (maximum power) velocity,  $V_{Pmax} = [2P_{max}/(c_p \rho A)]^{1/3}$ 
  - Power coefficient  $c_p$  = generator power divided by wind power
- Between  $V_{Pmax}$  and  $V_{cut-out}$  operate at maximum power

$$\bar{P}_{operation} = \int_{V_{cut-in}}^{V_{Pmax}} \frac{c_p \rho A V^3}{2} f(V) dV + \int_{V_{Pmax}}^{V_{cut-out}} P_{max} f(V) dV$$

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### Average Operating Power II

- Using power fraction table

$$\int_{V_{cut-in}}^{V_{Pmax}} \frac{c_p \rho A V^3}{2} f(V) dV = [f_P(V_{cut-in}) - f_P(V_{Pmax})] \frac{c_p \rho A c^3}{2} \Gamma\left(\frac{3}{k} + 1\right)$$

- Using cumulative distribution

$$\int_{V_{Pmax}}^{V_{cut-out}} P_{max} f(V) dV = P_{max} \left[ \left(1 - e^{-(V_{cut-out}/c)^k}\right) - \left(1 - e^{-(V_{Pmax}/c)^k}\right) \right]$$

$$\bar{P}_{operation} = [f_P(V_{cut-in}) - f_P(V_{Pmax})] \frac{c_p \rho A c^3}{2} \Gamma\left(\frac{3}{k} + 1\right) + P_{max} \left( e^{-(V_{Pmax}/c)^k} - e^{-(V_{cut-out}/c)^k} \right)$$

### Example Problem

- Data:  $k = 1.6$ ,  $c = 10$  m/s,  $V_{cut-in} = 5$  m/s,  $V_{Pmax} = 15$  m/s,  $V_{cut-out} = 25$  m/s
- $V_{cut-in}/c = (5 \text{ m/s}) / (10 \text{ m/s}) = 0.5$
- $V_{Pmax}/c = (15 \text{ m/s}) / (10 \text{ m/s}) = 1.5$
- $f_P(V_{Pmax}) - f_P(V_{cut-in}) = 0.328893 - 0.006295 = 0.322598$  (table next chart)

$$\Gamma\left(\frac{3}{k} + 1\right) = \Gamma\left(\frac{3}{1.6} + 1\right) = \Gamma(2.875) = (1.875)\Gamma(1.875)$$

$$= (1.875)(0.875)\Gamma(0.875)$$

### Use of Power Fraction Table

| Fraction of Wind Power Between $V = 0$ and Given $V$ |                                      |                 |           |          |           |           |
|--|--------------------------------------|-----------------|-----------|----------|-----------|-----------|
| $V/c$  | Fraction for Following Values of $k$ |                 |           |          |           |           |
|  | $k = 1.4$                            | $k = 1.6$       | $k = 1.8$ | $k = 2$  | $k = 2.2$ | $k = 2.4$ |
| 0.50   | 0.004948                             | <b>0.006295</b> | 0.007273  | 0.007877 | 0.008149  | 0.008156  |
| 0.60   | 0.010169                             | 0.013427        | 0.016118  | 0.018147 | 0.019530  | 0.020338  |
| 0.70   | 0.018369                             | 0.024959        | 0.030868  | 0.035837 | 0.039800  | 0.042794  |
| 0.80   | 0.030166                             | 0.041893        | 0.053010  | 0.063024 | 0.071728  | 0.079088  |
| 0.90   | 0.046036                             | 0.064971        | 0.083615  | 0.101180 | 0.117277  | 0.131769  |
| 1.00   | 0.066279                             | 0.094589        | 0.123163  | 0.150855 | 0.177061  | 0.201517  |
| 1.10   | 0.091003                             | 0.130760        | 0.171457  | 0.211508 | 0.250044  | 0.286651  |
| 1.20   | 0.120122                             | 0.173115        | 0.227629  | 0.281520 | 0.333573  | 0.383162  |
| 1.30   | 0.153376                             | 0.220943        | 0.290233  | 0.358382 | 0.423715  | 0.485322  |
| 1.40   | 0.190353                             | 0.273260        | 0.357401  | 0.439009 | 0.515849  | 0.586691  |
| 1.50   | 0.230519                             | <b>0.328893</b> | 0.427029  | 0.520117 | 0.605340  | 0.681244  |

### Gamma Function Table

| Abridged Table of Gamma Functions |             |      |             |             |                 |
|-----------------------------------|-------------|------|-------------|-------------|-----------------|
| $x$                               | $\Gamma(x)$ | $x$  | $\Gamma(x)$ | $x$         | $\Gamma(x)$     |
| 0.01                              | 99.43259    | 0.16 | 5.81127     | 0.40        | 2.21816         |
| 0.02                              | 49.44221    | 0.18 | 5.13182     | 0.45        | 1.968136        |
| 0.03                              | 32.78500    | 0.20 | 4.59084     | 0.50        | 1.772454        |
| 0.04                              | 24.46096    | 0.22 | 4.15048     | 0.55        | 1.616124        |
| 0.05                              | 19.47009    | 0.24 | 3.78550     | 0.60        | 1.489192        |
| 0.06                              | 16.14573    | 0.26 | 3.47845     | 0.65        | 1.384795        |
| 0.07                              | 13.77360    | 0.28 | 3.21685     | 0.70        | 1.298055        |
| 0.08                              | 11.99657    | 0.30 | 2.99157     | 0.75        | 1.225417        |
| 0.09                              | 10.61622    | 0.32 | 2.79575     | 0.80        | 1.16423         |
| 0.10                              | 9.51351     | 0.34 | 2.62416     | <b>0.85</b> | <b>1.112484</b> |
| 0.11                              | 8.61269     | 0.36 | 2.47273     | <b>0.90</b> | <b>1.068629</b> |
| 0.12                              | 7.86325     | 0.38 | 2.33826     | 0.95        | 1.031453        |
| 0.13                              | 7.23024     |      |             |             |                 |
| 0.14                              | 6.68669     |      |             |             |                 |

Interpolate for  $\Gamma(0.875) = 1.0905565$

$\Gamma(2.875) = (1.875)(0.875) = (1.875)(0.875) = (1.0905565) = 1.789$

### Example II

- Computations below rated speed

$$\frac{1}{A} [f_P(V_{Pmax}) - f_P(V_{cut-in})] \frac{c_p \rho A c^3}{2} \Gamma\left(\frac{3}{k} + 1\right) = [0.322598]$$

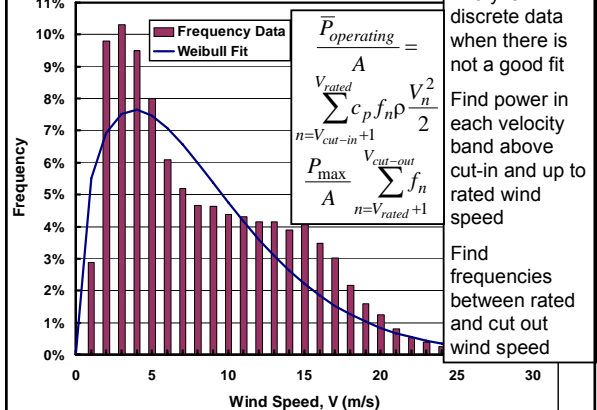
$$\frac{0.48 \cdot 1.225 \text{ kg} \cdot (10 \text{ m})^3}{2 \text{ m}^3} \left(\frac{10 \text{ m}}{\text{s}}\right)^3 (1.789) \frac{1 \text{ W} \cdot \text{s}^3}{\text{kg} \cdot \text{m}^2} = \frac{526.0 \text{ W}}{\text{m}^2}$$

- Computations above rated speed

$(V_{cut-out}/c = 2.5)$  give  $0.1345 P_{max}$

$$P_{max} \left( e^{-(V_{Pmax}/c)^k} - e^{-(V_{cut-out}/c)^k} \right) = P_{max} \left[ e^{-(1.5)^{1.6}} - e^{-(2.5)^{1.6}} \right]$$

### Weibull Fit Comparison



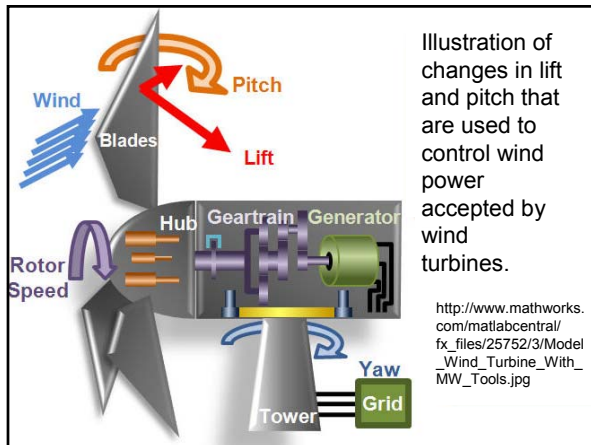
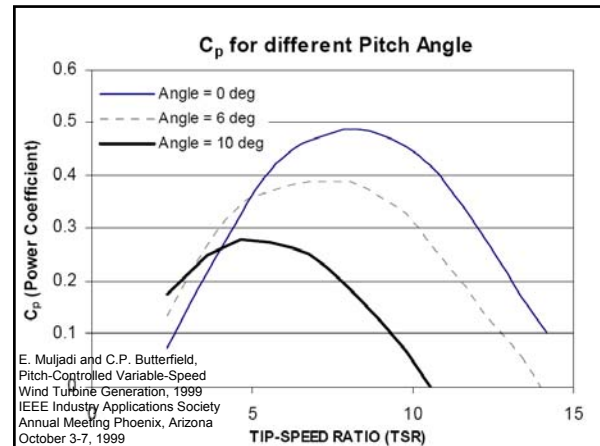
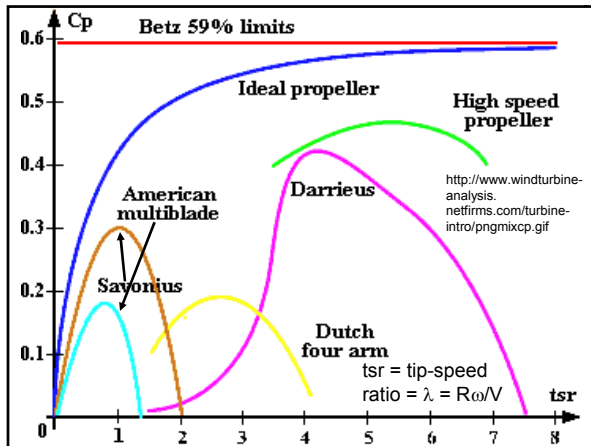
$$\bar{P}_{operation} = \frac{A}{\sum_{n=V_{cut-in}+1}^{V_{rated}} c_p f_n \rho \frac{V_n^2}{2}}$$

$$\frac{P_{max}}{A} \sum_{n=V_{rated}+1}^{V_{cut-out}} f_n$$

Analyze discrete data when there is not a good fit

Find power in each velocity band above cut-in and up to rated wind speed

Find frequencies between rated and cut out wind speed



### Turbine Power Controls

- Pitch controls – adjusts the angle of the **movable** blades (pitch)
  - Reduces fraction of power extracted from wind, keeping generator power constant
- Passive stall controls design the angle of the **fixed** rotor blades to reduce lift force at higher wind speeds
  - Maintains constant force on rotor shaft as wind speed increases above maximum

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### Turbine Power Controls II

- Passive stall control
  - uses basic rotor design to ensure proper control
  - no changes in rotor blades' position during operation
- Active stall control
  - Changes blade pitch to increase stall force in a manner similar to pitch control

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### Environmental Impacts

- Visual impact
- Noise
- Effect on birds (avian impacts)
- Electromagnetic interference
- Bats
- Not discussed
  - Environmental benefits in reduction of fossil-fuel generated pollutants, including greenhouse gas CO<sub>2</sub>

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